

MASS TIMBER IN PRACTICE

Progress in Educational Buildings
and the Building Code

Joe Mayo, AIA LEED AP
Mahlum Architects

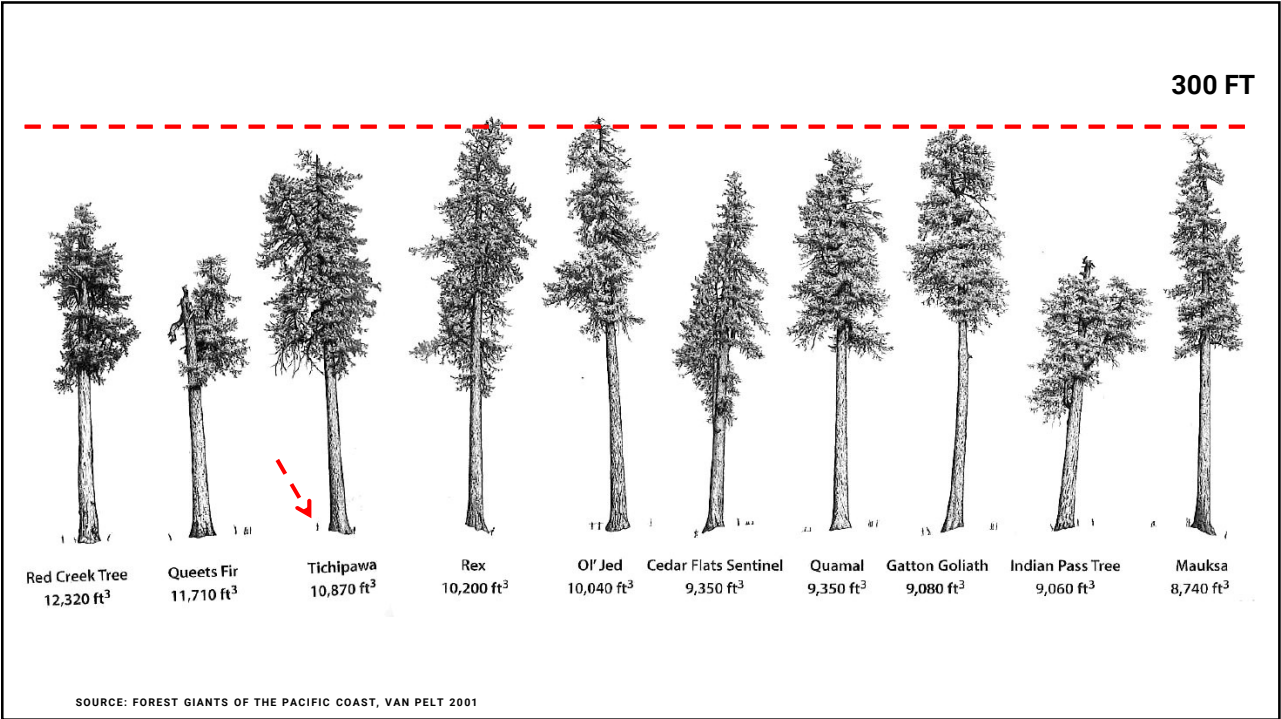


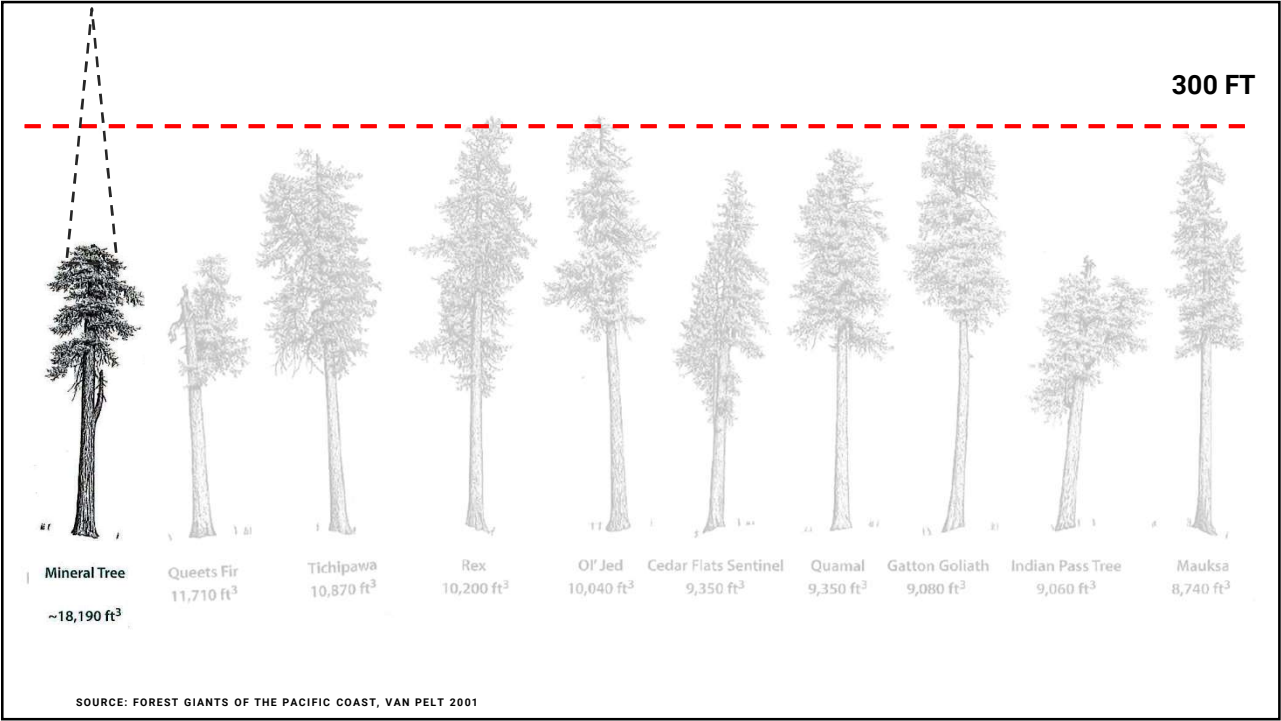
**Mahlum envisions a world where healthy
human and environmental systems thrive.**

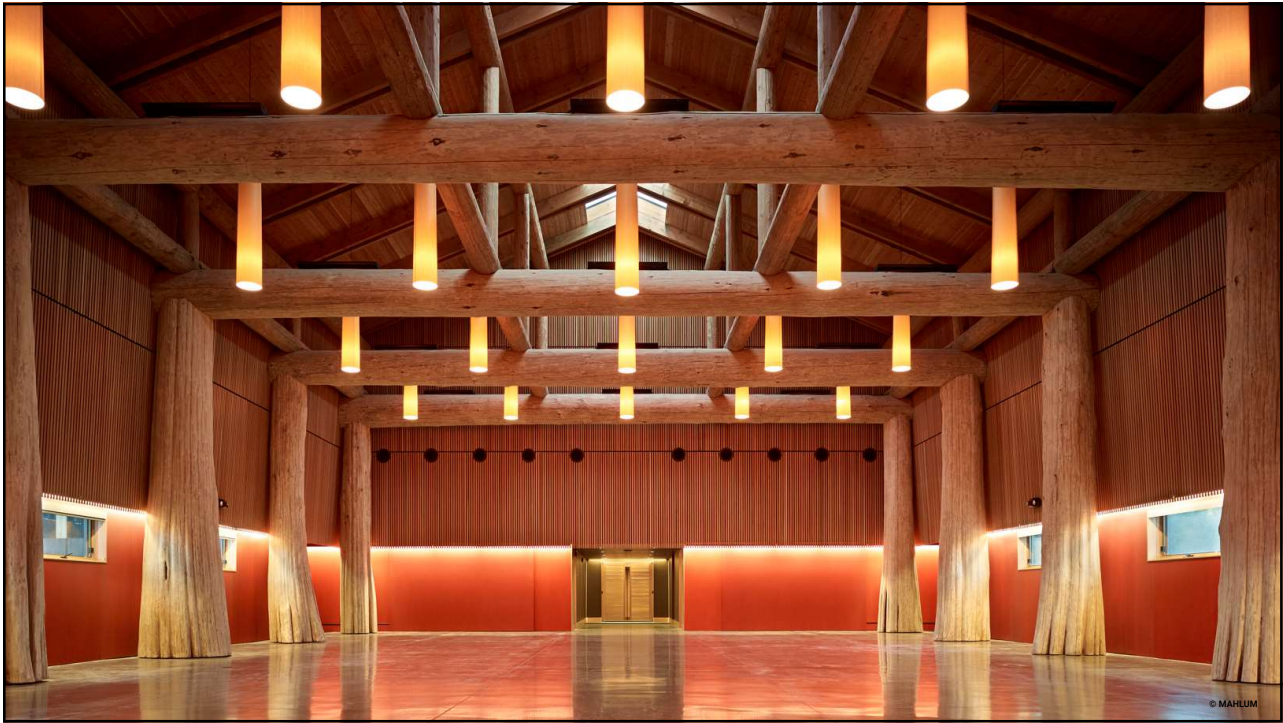
We believe community empowerment will be the game-changing force
that leads to sustainable, transformational ways to make that possible.

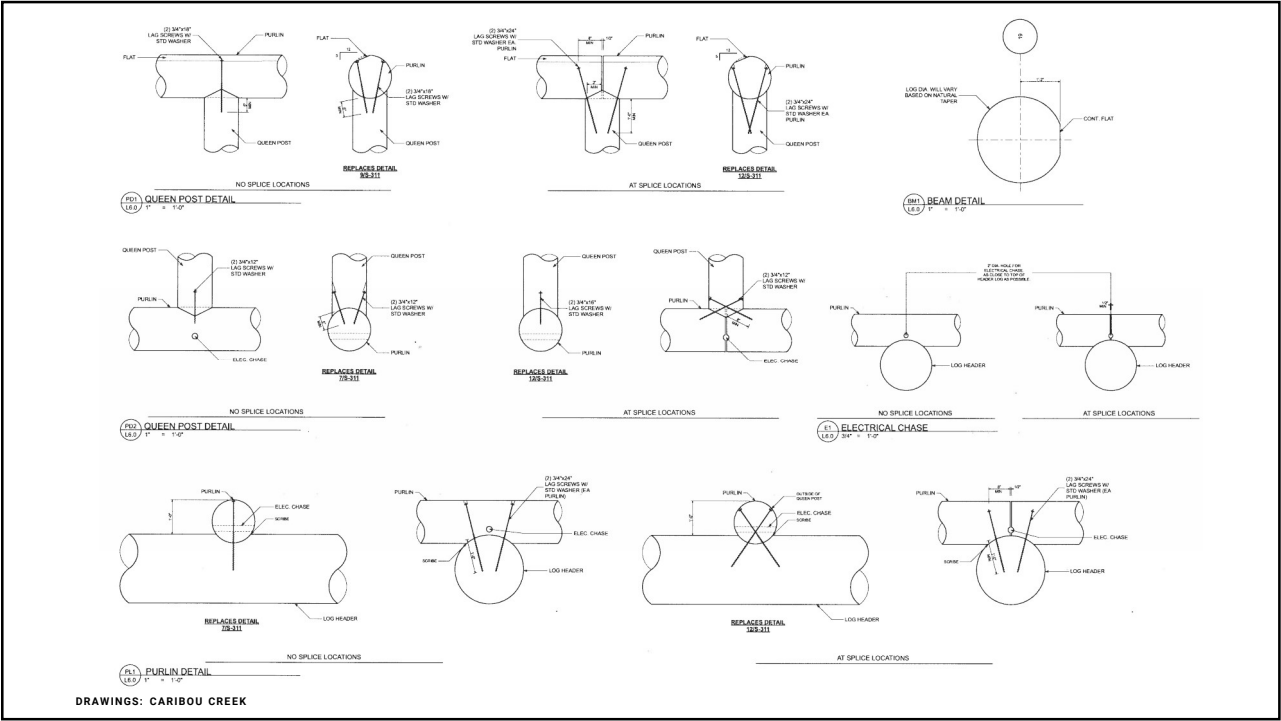
The Pacific Northwest

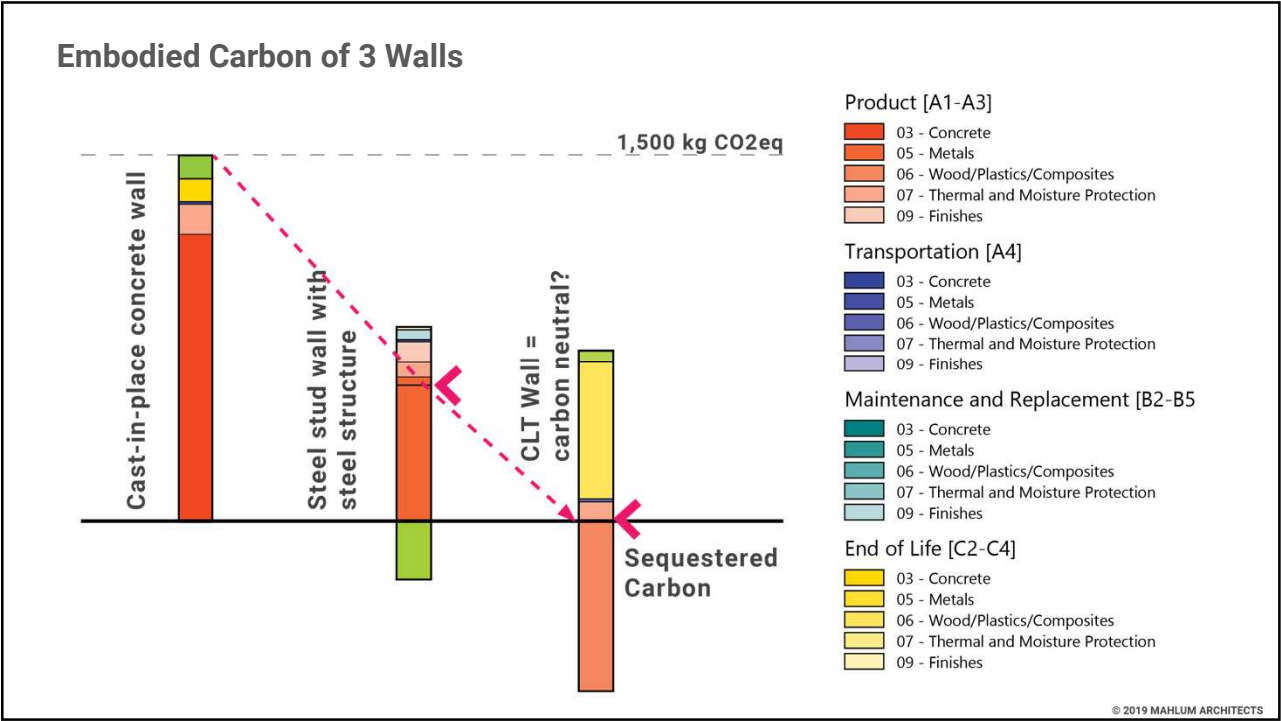
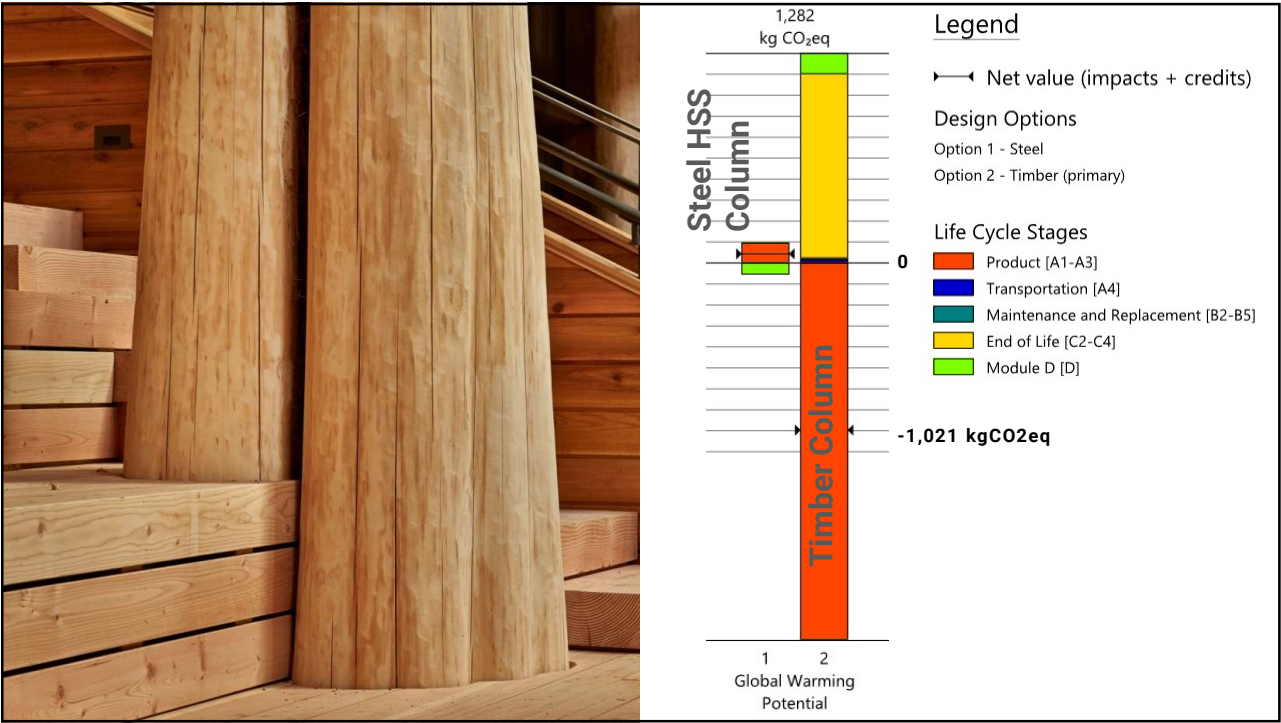
Can a building embody a culture?
(in the age of climate change)











Richard Woodcock Center for Education
How do we actually use CLT?
2015-2016

At-a-Glance

Location:
**Western Oregon
University,
Monmouth, Oregon**

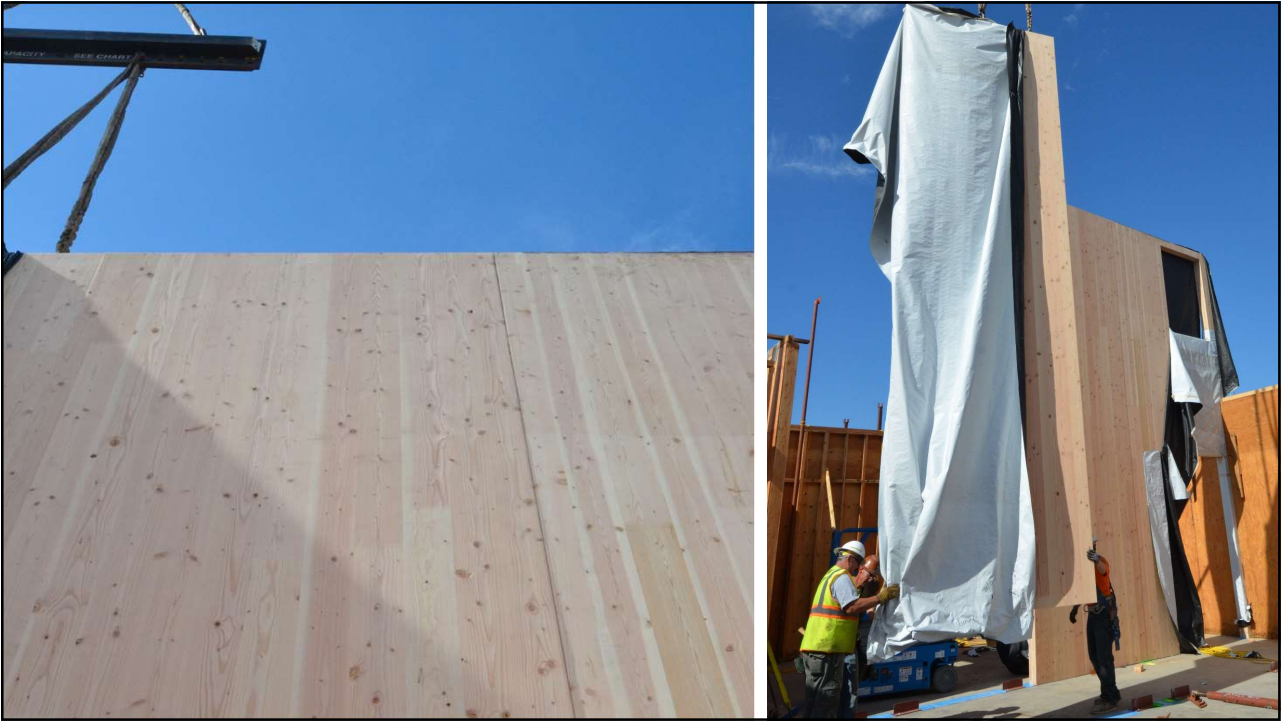
Area:
52,000 SF

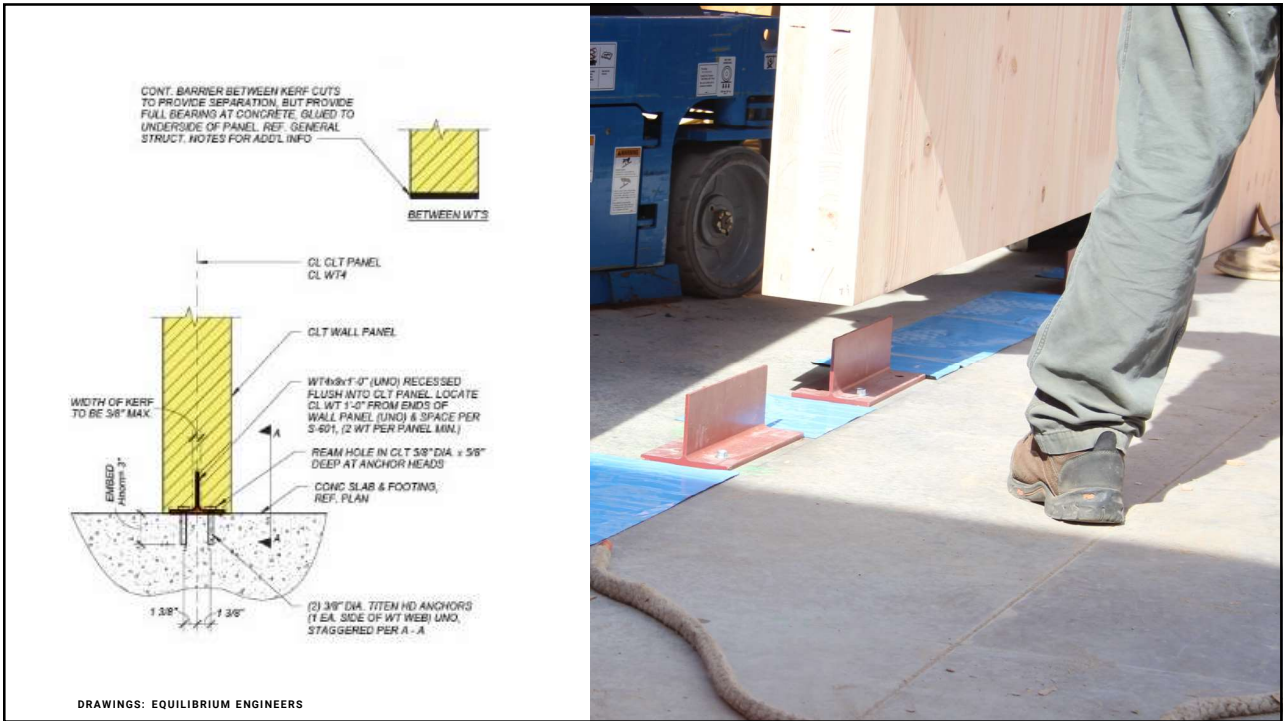
Height:
2-stories (~45' tall)

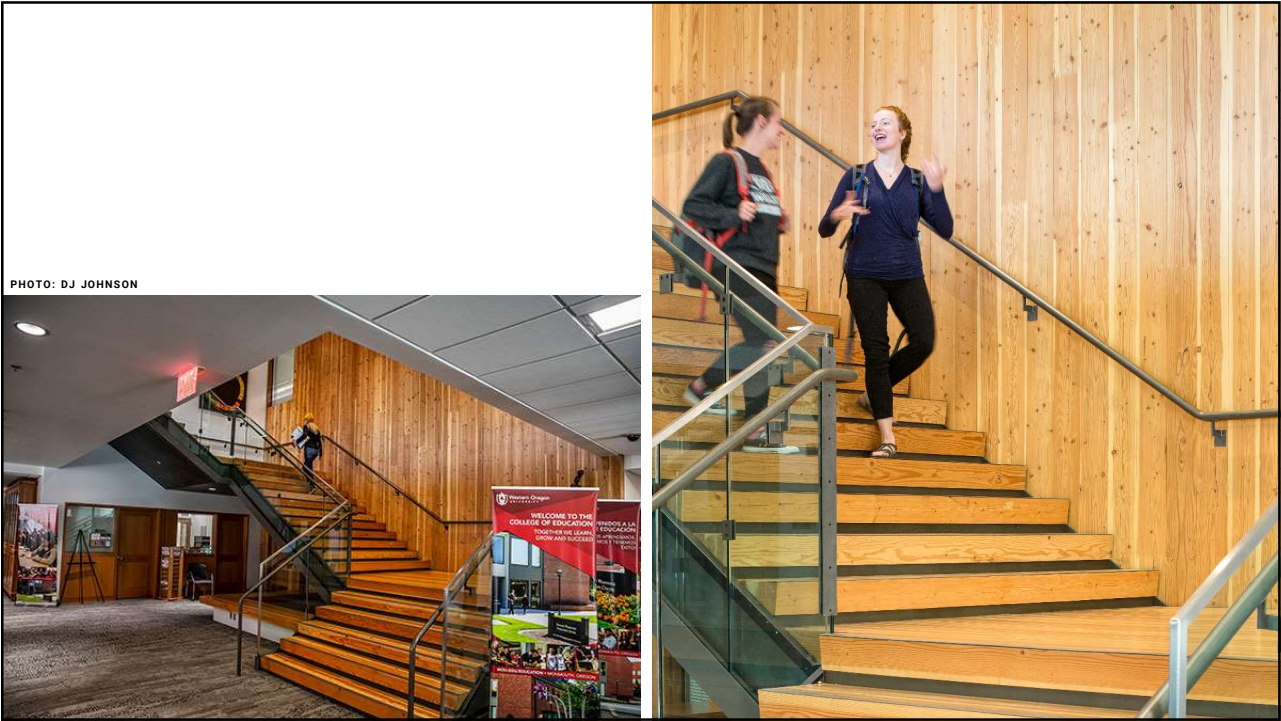
Occupancy: **B**

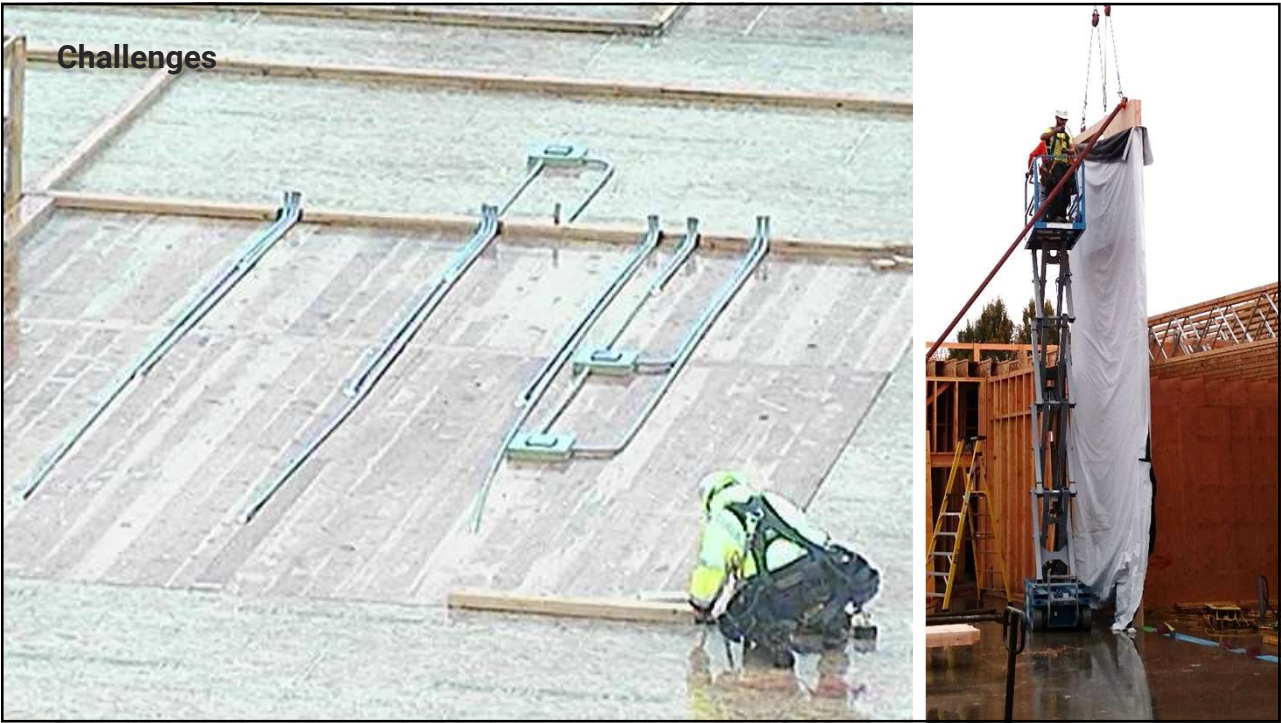
Construction:
Type VB

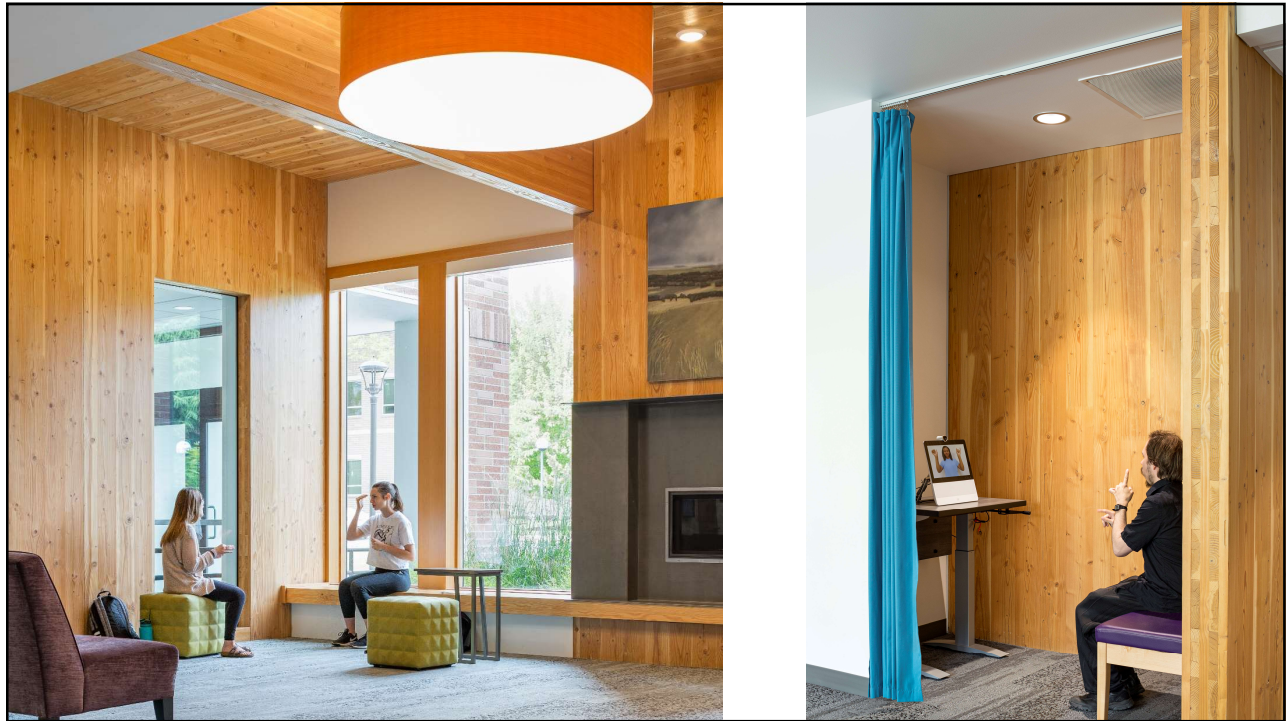












CLT Pilot Program Classrooms
**Can a small project be a catalyst
 to revitalize Washington State's
 rural economy?**
 2016-2017



At-a-Glance

3 unique school districts and sites

Provided appropriation:
About \$250K per classroom
(Comparable to a portable)

Provide improved learning environment and durability

Reduce K-3 class size
(Students per teacher ratio)

Utilize as much CLT as possible

Test Progressive Design-Build Project Delivery Method

Fast-track schedule:
13 months to design, document and build 3 classroom buildings


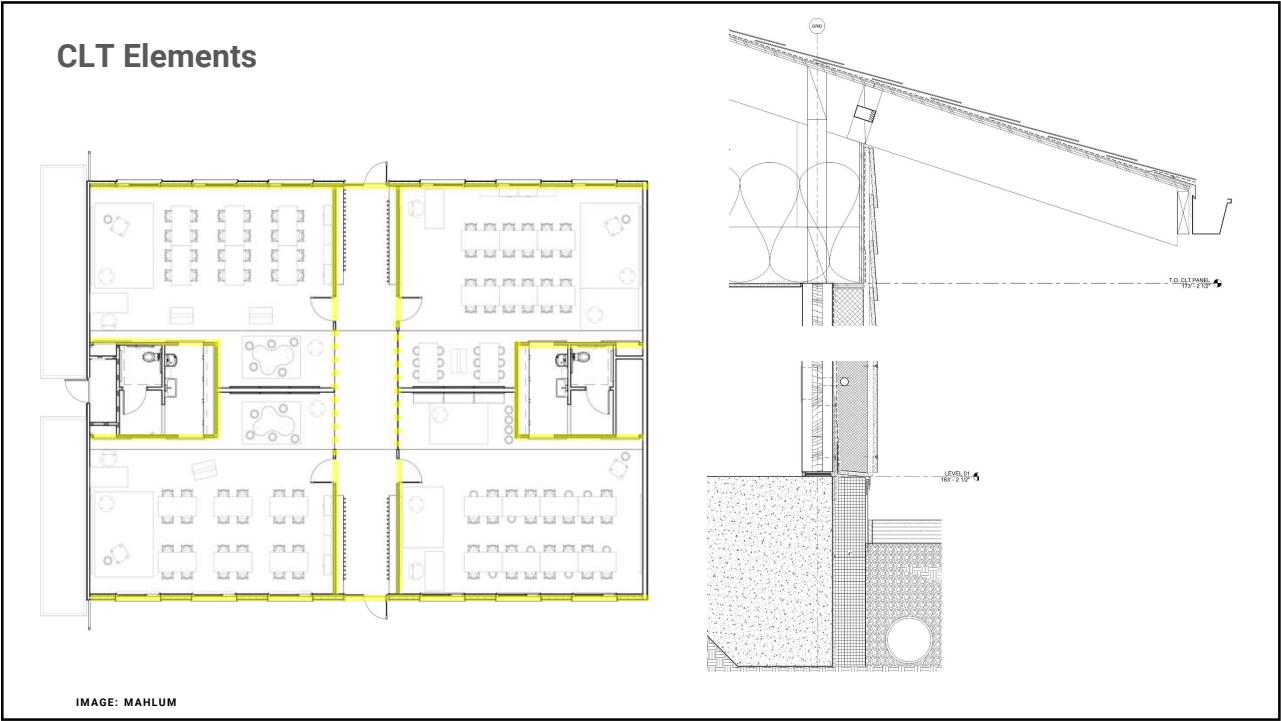
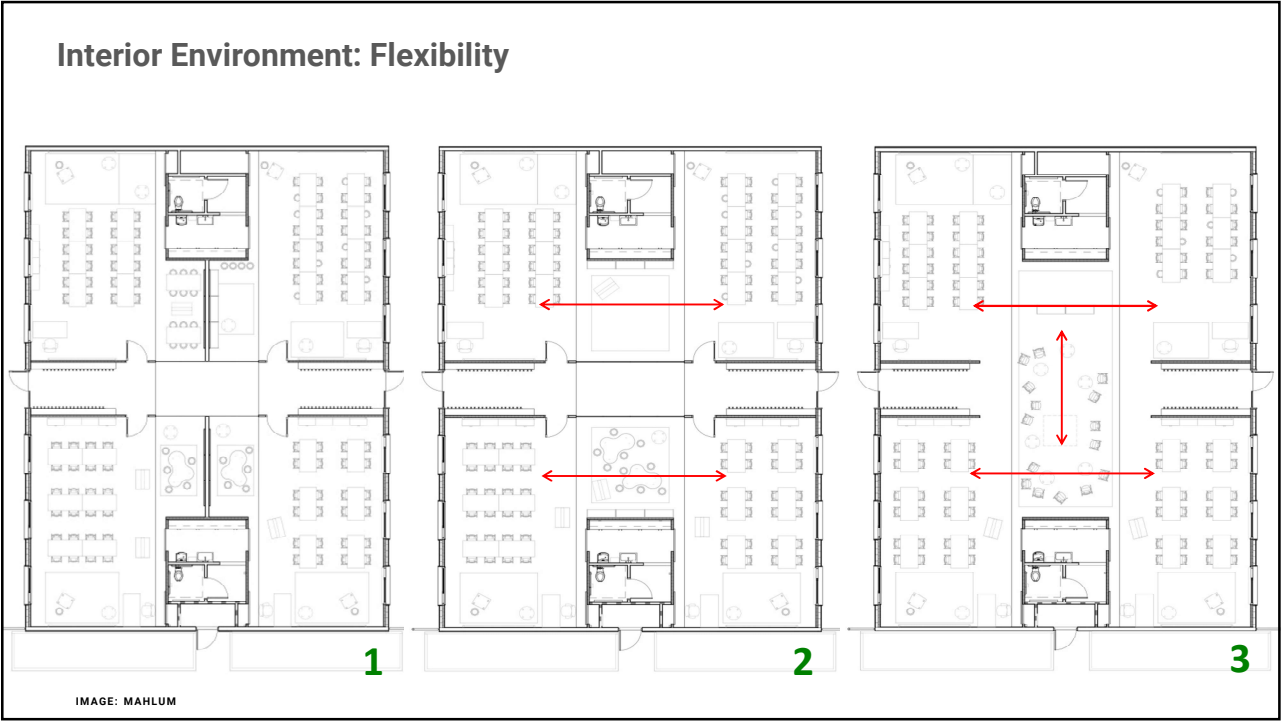


IMAGE: MAHLUM



Structural: CLT as Lateral Force Resisting System

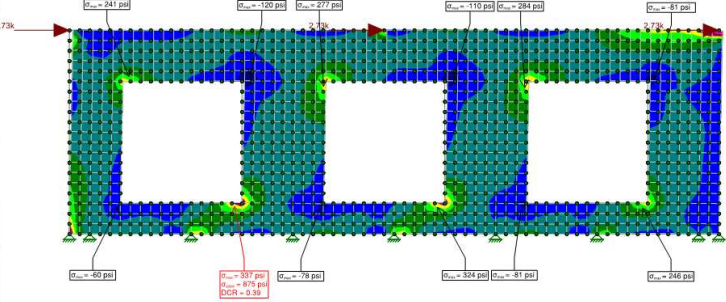


Diagram illustrating the structural behavior of CLT as a lateral force resisting system. The diagram shows a cross-section of a CLT wall and diaphragm assembly under lateral load. The wall is subjected to a lateral load of 7.7k. The diaphragm is subjected to a lateral load of 2.7k. The diagram shows the distribution of shear stress and the location of fasteners. The fastener requirements are listed as follows:

- Top edge: $C_{w,1} = 241 \text{ psi}$, $C_{w,2} = 120 \text{ psi}$, $C_{w,3} = 277 \text{ psi}$, $C_{w,4} = 110 \text{ psi}$, $C_{w,5} = 284 \text{ psi}$, $C_{w,6} = 81 \text{ psi}$
- Bottom edge: $C_{b,1} = 50 \text{ psi}$, $C_{b,2} = 301 \text{ psi}$, $C_{b,3} = 975 \text{ psi}$, $C_{b,4} = 78 \text{ psi}$, $C_{b,5} = 324 \text{ psi}$, $C_{b,6} = 81 \text{ psi}$, $C_{b,7} = 246 \text{ psi}$

DCR = 0.39

2 SHEAR WALLS AND DIAPHRAGMS

Resistance to lateral loads from wind and earthquakes in CLT structures is made through wall and floor panels designed as shear walls and diaphragms. Unlike typical wood-frame shear wall and diaphragm systems, which have design unit shear strength prescribed based on a specific construction (AWC, 2008), the design shear strength of CLT shear walls and diaphragms is determined directly based on principles of engineering mechanics using provisions of the National Design Specification (NDS) for Wood Construction (AWC, 2012) for connection design (see Chapter 5 entitled *Connections in cross-laminated timber buildings*) and CLT panel design (see Chapter 3 entitled *Structural design of cross-laminated timber elements*). The unit shear strength of the CLT shear wall and CLT diaphragm will vary by factors such as fastener size, spacing, and location as well as the shear strength of the CLT panel itself. Deflection estimates based on principles of engineering mechanics or derived from testing should account for all sources of deflection including panel bending, panel and/or connector shear, and fastener deformation.

Capacity design principles are recommended for design of CLT for seismic resistance to ensure predictable yielding in CLT wall panels and interconnection of CLT elements through fastener yielding, wood crushing, or a combination thereof prior to onset of undesirable brittle wood failure modes. This approach recognizes that wall panel-to-panel and panel-to-floor connections provide the primary source of yielding, while the wood wall panels themselves remain essentially elastic. Special seismic detailing of the CLT seismic force resisting system includes the following:

See page 3

- a) **Fastener Requirements.** Fasteners loaded in shear are designed such that the expected fastener yield mode is Mode III or Mode IV as defined in the NDS.
- b) **CLT Member Design at Connections.** The nominal connection capacity determined in accordance with Item c) is used as the minimum design demand for any wood member limit states.
- c) **Nominal Connection Capacity.** The nominal connection capacity in shear is determined in accordance with the following:
For dowel type fasteners $- n \times Z(K_1)(C_{w,1})(C_{w,2})(C_{w,3})$ where n is the number of fasteners; Z is the reference lateral design value for a single fastener; and K_1 , $C_{w,1}$, $C_{w,2}$, and $C_{w,3}$ are adjustment factors specified in the NDS for format conversion, time effect, wet service, temperature and end grain, respectively.
- d) **Fastener Withdrawal.** Where a connector relies directly on fastener withdrawal for load resistance, testing shall demonstrate that the fasteners can develop substantial yielding in the connector prior to full fastener withdrawal.

IMAGE: COUGHLIN PORTER LUNDEEN

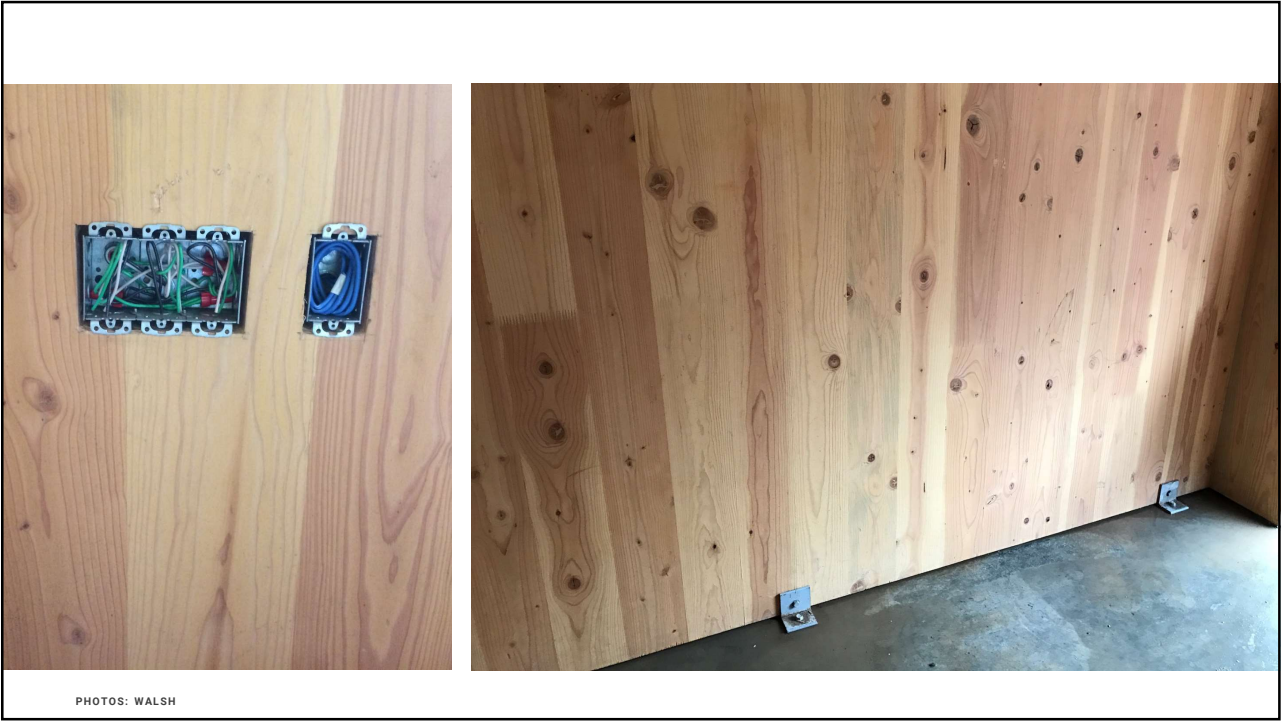
Local Wood

Interfor Mill, Port Angeles, Washington



IMAGE: INTERFOR MILL





Cost: State-Wide Study (2017)

WASHINGTON STATE OFFICE OF THE SUPERINTENDENT OF PUBLIC INSTRUCTION
K-12 CAPITAL FACILITIES COST STUDY

4.2 WASHINGTON STATE COST RANGE BY SCHOOL TYPE

Based on the cost range by space program, a statewide average range of construction costs were developed for each school type. Construction costs exclude Washington State sales tax, site costs, and indirect costs. A project allowance has been added to the table below to reach the total project cost that includes a range of typical site costs and indirect costs. Costs outside of the typical range for special or extraordinary conditions are not included.

NEW DIRECT CONSTRUCTION*	Elementary		Middle		High	
	Low Cost/GSF	High Cost/GSF	Low Cost/GSF	High Cost/GSF	Low Cost/GSF	High Cost/GSF
Washington State Average	\$230	\$309	\$246	\$326	\$265	\$344
Add Site Costs Allowance	10.0%	12.0%	10.0%	15.0%	10.0%	15.0%
Add Indirect Costs Allowance	25.0%	30.0%	30.0%	35.0%	30.0%	35.0%
	\$316	\$450				

Cost: CLT Classrooms vs Portables (2017)

CLT CLASSROOMS COST DATA			
	CLT Classrooms w/o site utilities (west side projects in Washington)	CLT Classrooms w/ site utilities (west side projects in Washington)	Traditional Modular (estimate)
Project Cost	\$2,758,000	\$2,978,000	-
Markups	\$137,900	\$148,900	-
Total	\$2,895,900	\$3,126,900	-
Per Building	\$965,300	\$1,042,300	-
Per Classroom	\$241,325	\$260,575	~\$250,000
Cost/SF (building)	\$247.51	\$267.26	-

Cost of a Double Portable

\$500,000

Manufacturing: \$200,000
Budget for siting: \$300,000

How Much Does a Portable Classroom Cost?

4,947 views

BethelSchools
Published on Aug 24, 2016

SUBSCRIBE 1.4K

VIDEO: YOUTUBE
BETHEL SCHOOL DISTRICT

Western Washington University
**Can CLT expedite
housing construction?**
2019-Current

At-a-Glance

Location:
Bellingham, Washington

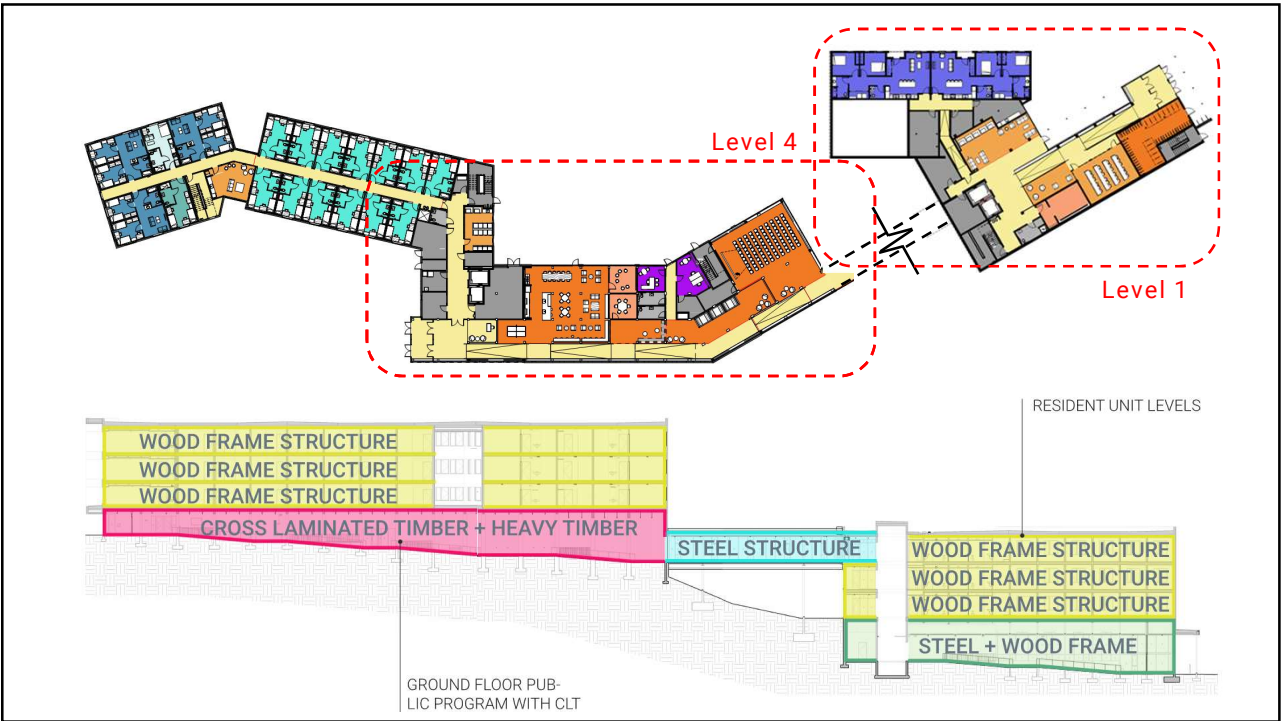
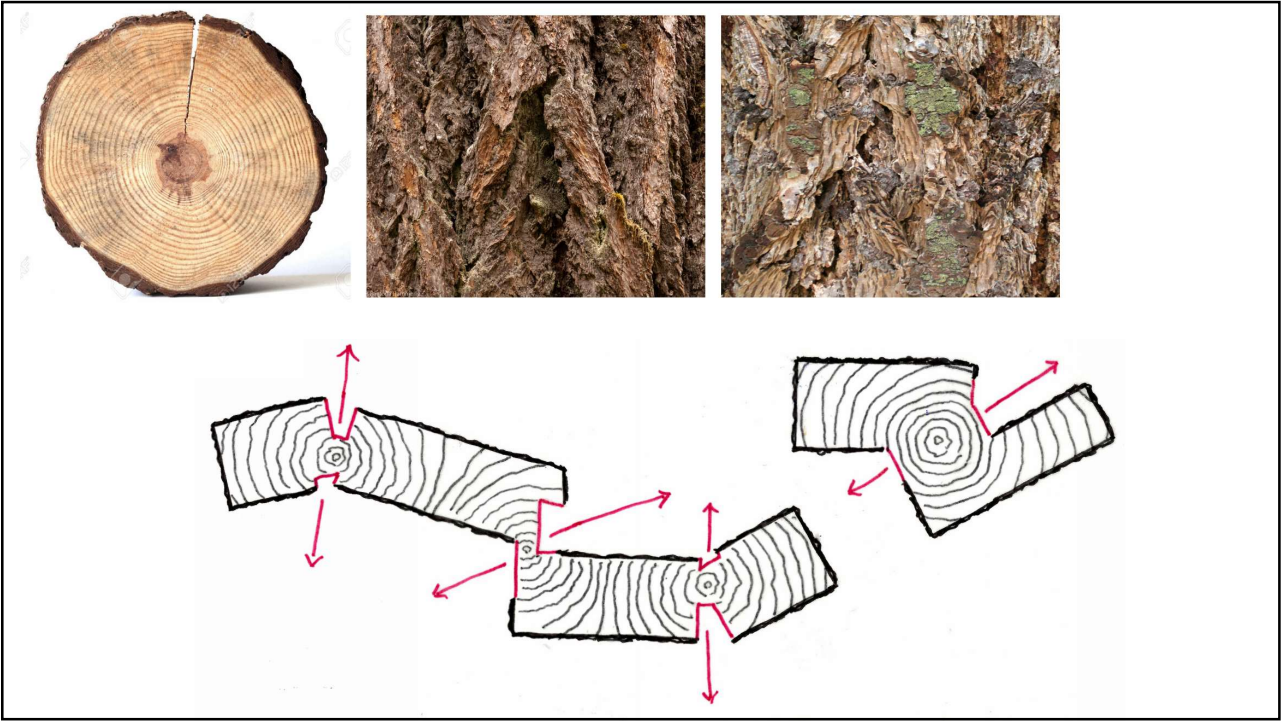
Area:
110,300 SF

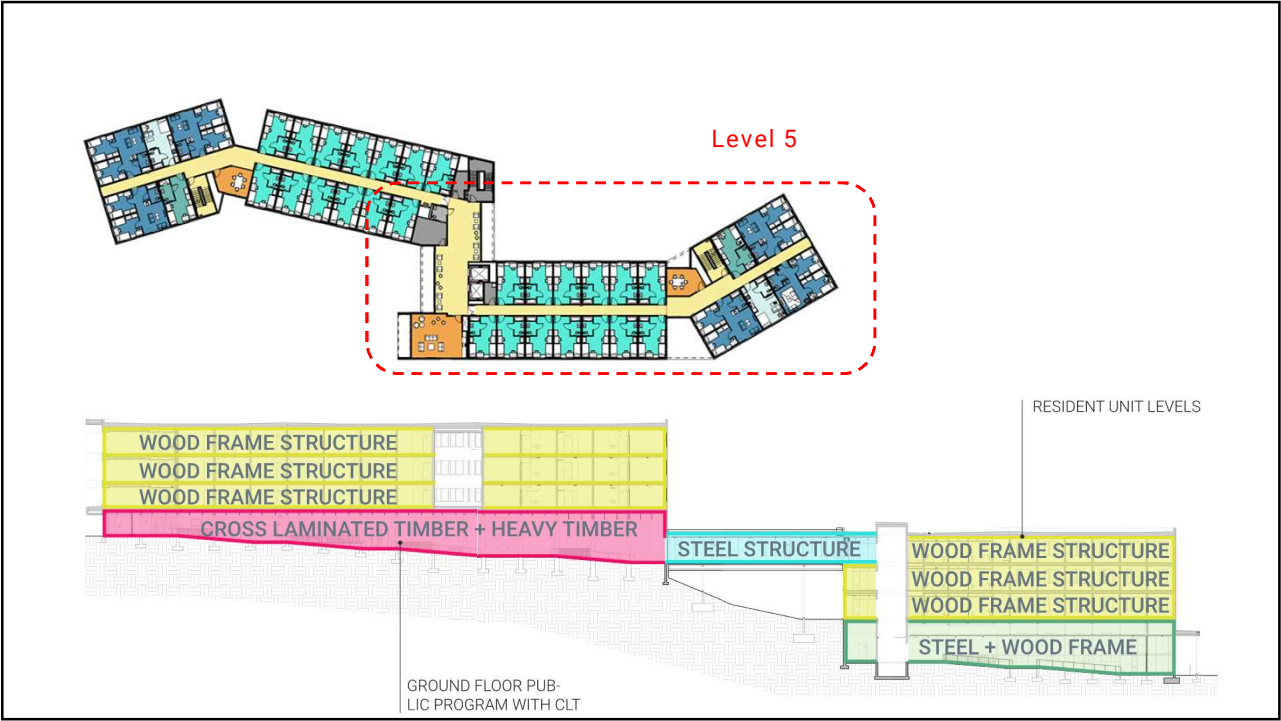
Height:
7-stories (~55-60' tall)

Occupancy: **R-2**

Construction Type: **VA**

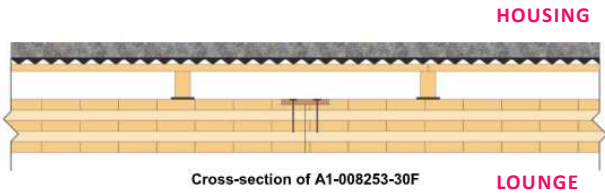








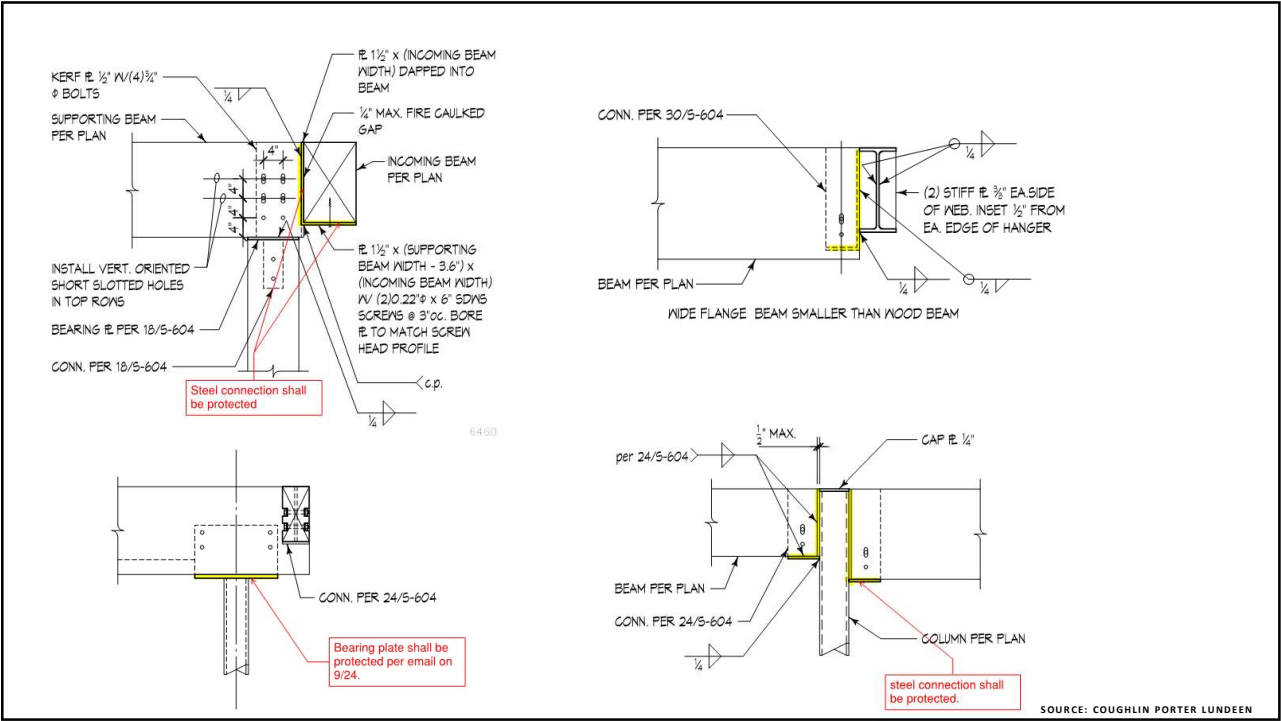
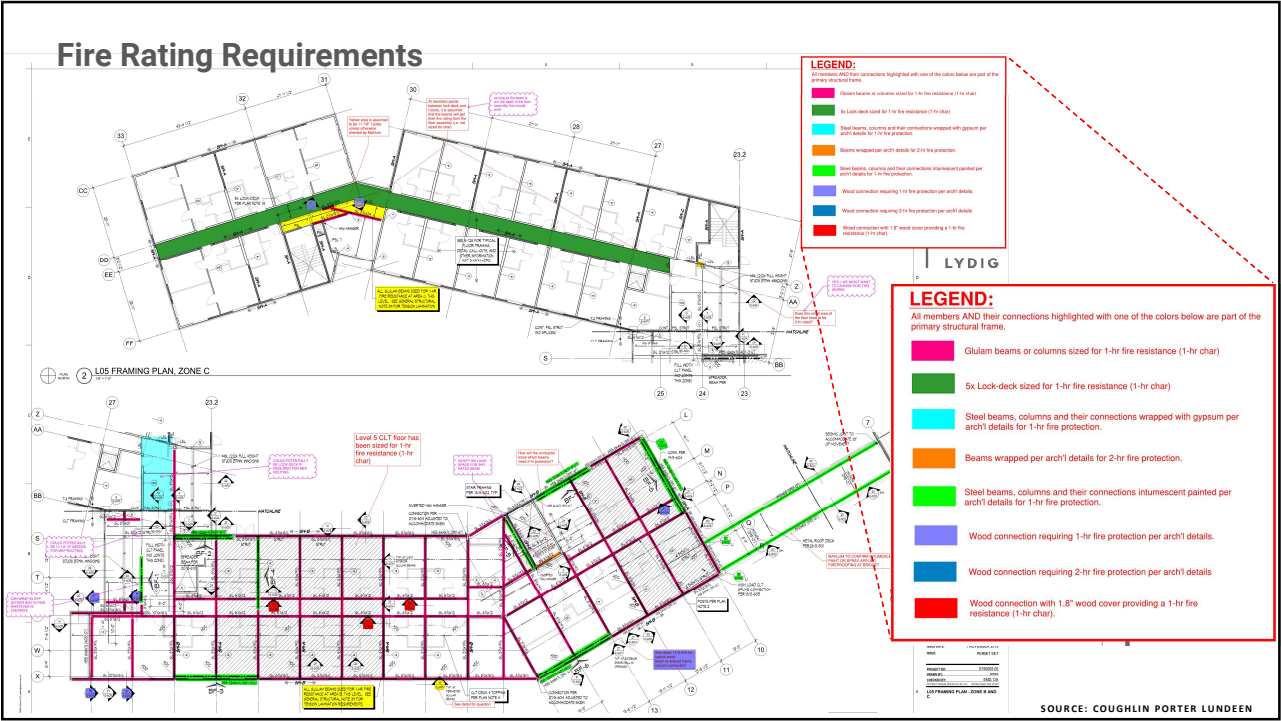
Tested Assembly: STC 59 (1.5” concrete)
Proposed Assembly: STC 56 (1.5” gypcrete)



Specimen Properties

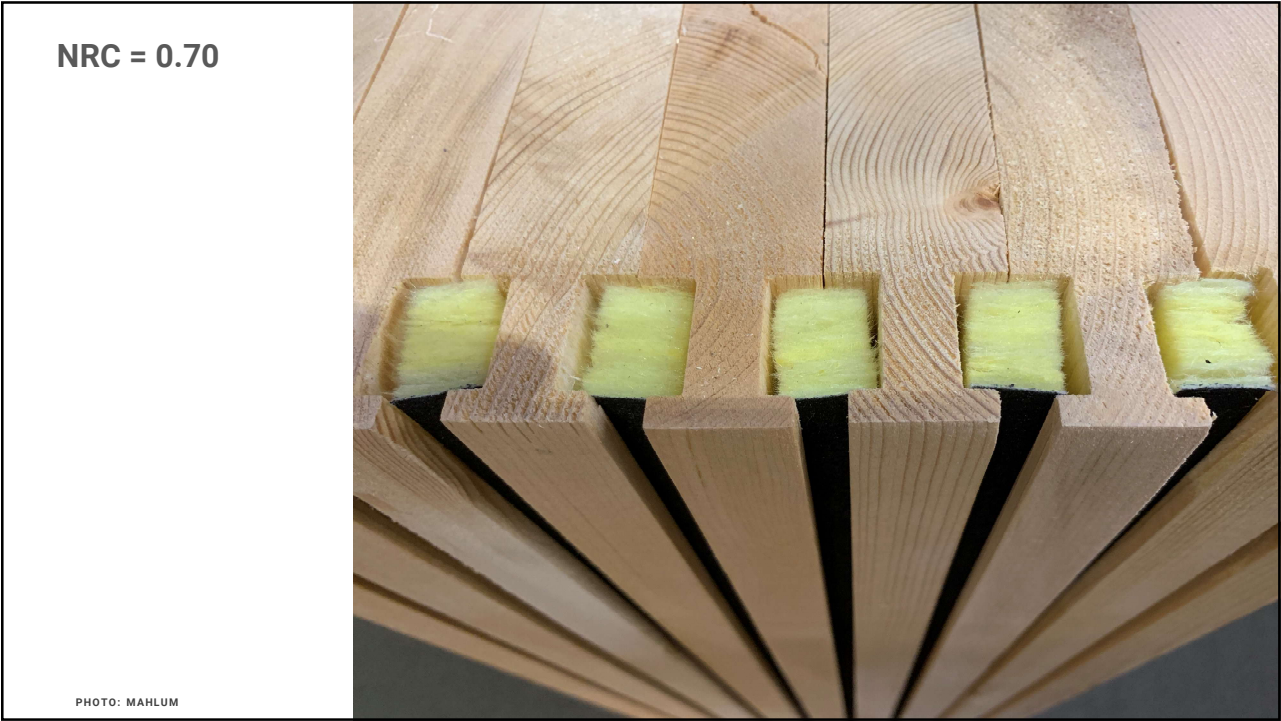
Element	Actual thickness (mm)	Mass (kg)	Mass/length, area or volume
38 mm Precast Concrete Slab	38	1 905	98.6 kg/m ²
17 mm Regupol® SonusWave™	17	157	8.1 kg/m ²
18 mm OSB Tongue and Groove Sheeting	18	202	10.5 kg/m ²
38 mm x 64 mm Wood Battens	64	47	0.3 kg/m
10 mm Rubber Membrane	10	21	7.7 kg/m ²
131 mm CLT 5 ply	131	1 343	69.3 kg/m ²
Total	278	3 675	190.2 kg/m ²

SOURCE: A3 ACOUSTICS



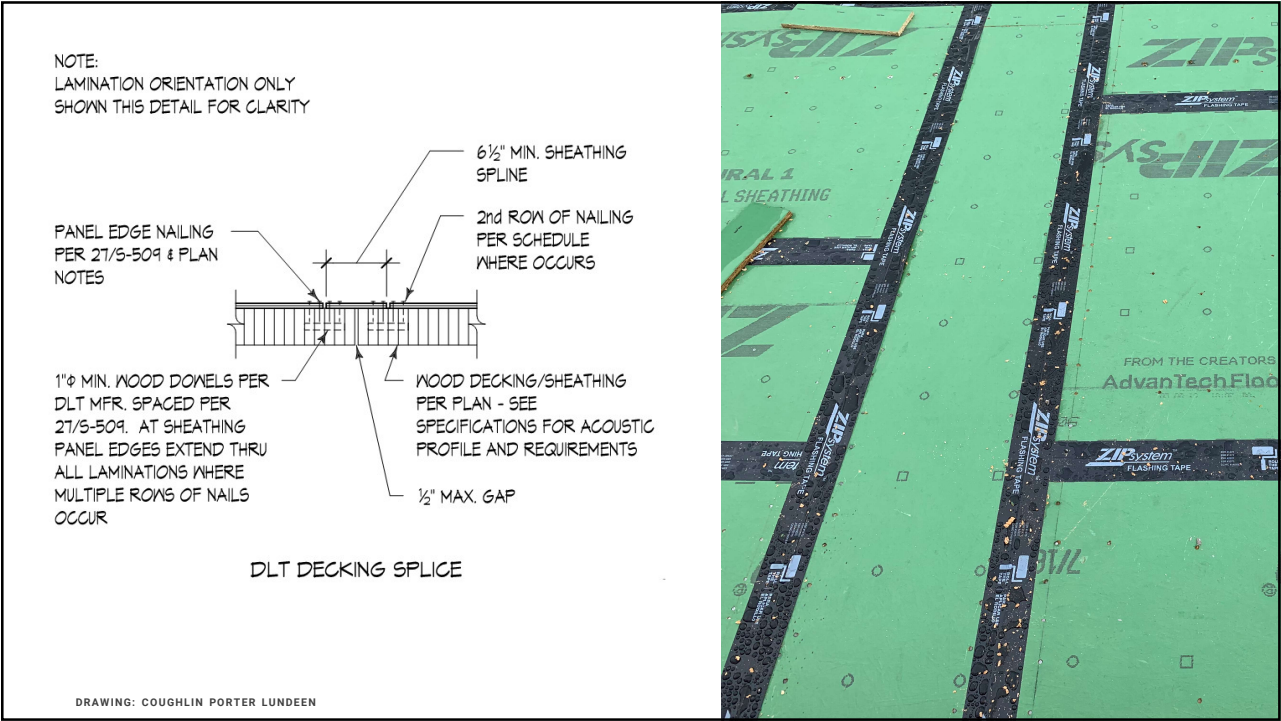
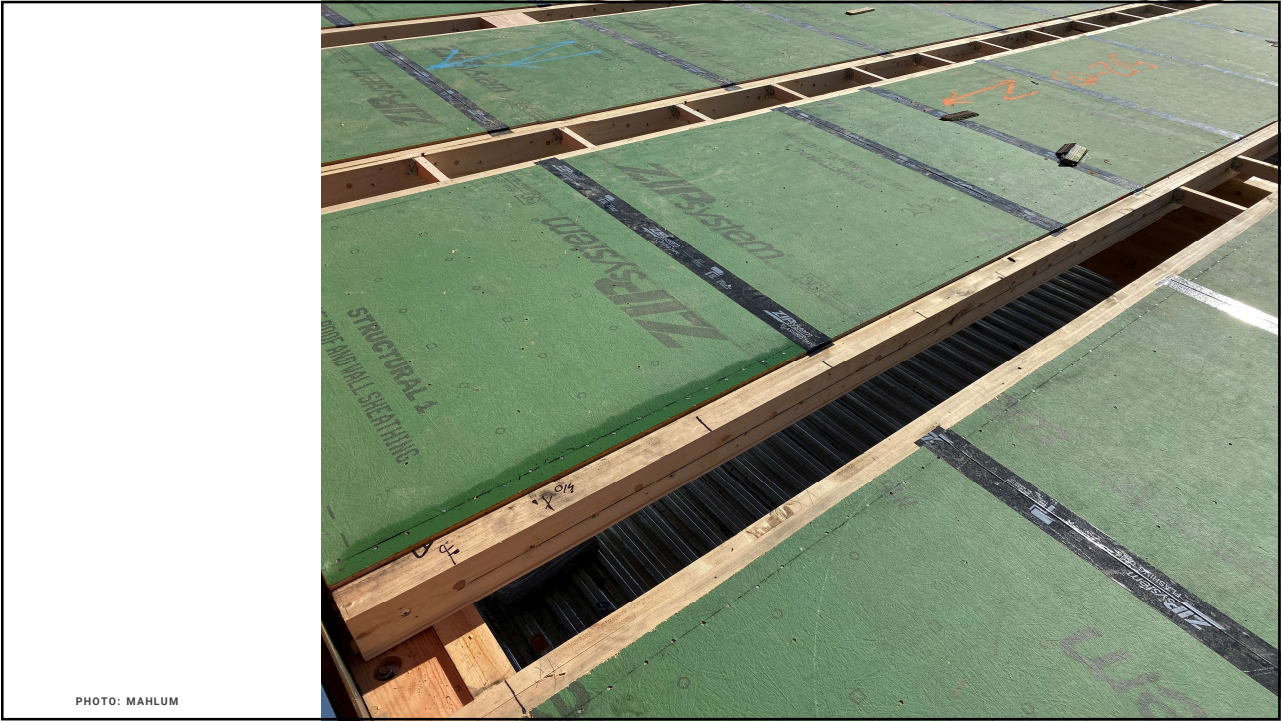


Kellogg Middle School
**First Acoustic DLT Installation
in the U.S.**
2017-Current









Design

DIAPHRAGM SHEATHING NAILING SCHEDULE				
ZONE	PANEL EDGE NAILING SPACING		SWG SCREW SPACING	WOOD DOWEL SPACING
	a	b		
	6'00	6'00	12'00	18'00
	3'00	4'00	12'00	15'00
	2½'00	2½'00	7½'00	10'00
	(2) ROWS @ 3'00	(2) ROWS @ 4'00	6'00	8'00

CHART: COUGHLIN PORTER LUNDEEN

Shop Drawing

DIAPHRAGM SHEATHING NAILING SCHEDULE			SCREW REINFORCING SCHEDULE	
ZONE	PANEL EDGE NAILING SPACING	SCREW SPACING	SCREW REINFORCING AT SPLINE ASSY VG (FT-CL) 85/16" x 9 1/2"	SCREW REINFORCING AT BUILDING EDGE ASSY VG (FT-CL) 83/8" x 11 3/4"
	A			
	6" O.C	12" O.C	11" O.C. @45 DEG ALTERNATE	18" O.C. @90 DEG INTO SIDE OF PANEL. SCREWS TO BE ALIGNED WITH DOWELS
	3" O.C	12" O.C	9" O.C. @45 DEG ALTERNATE	
	2-1/2" O.C	7-1/2" O.C	5" O.C. @45 DEG ALTERNATE	
	(2) ROWS @ 3" O.C	6" O.C	10" O.C. @45 DEG ALTERNATE	

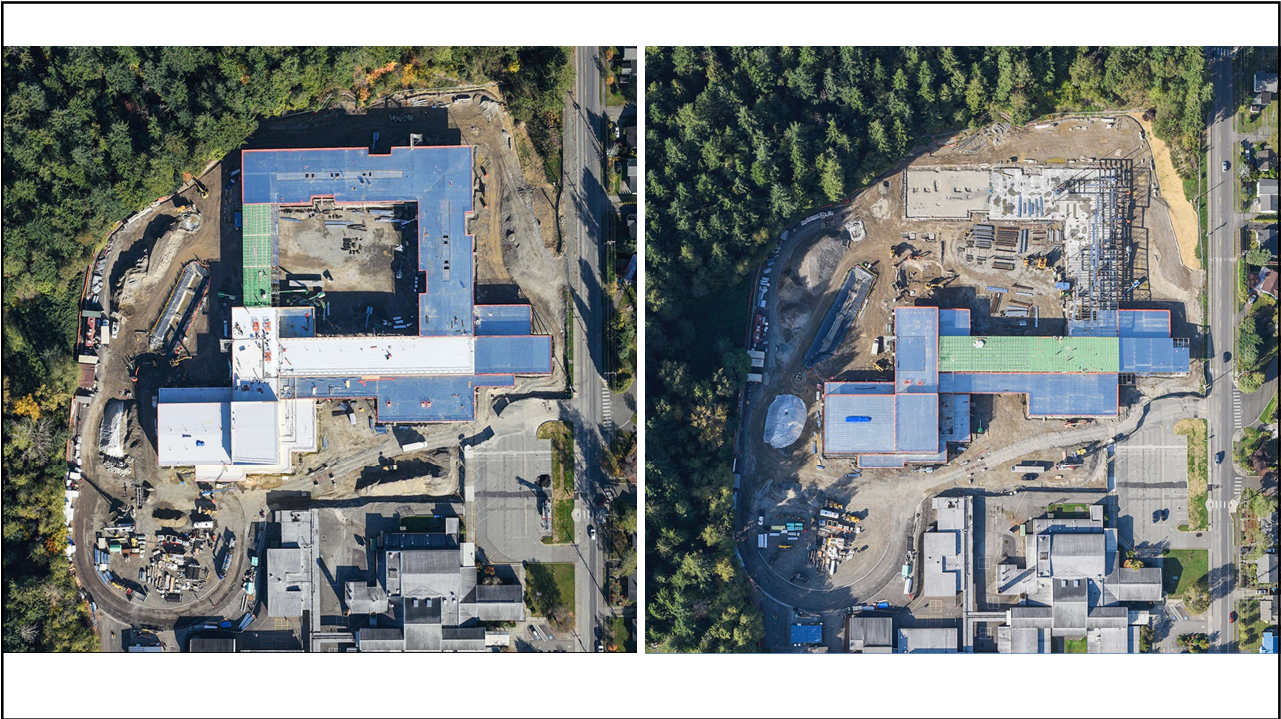
NOTES:

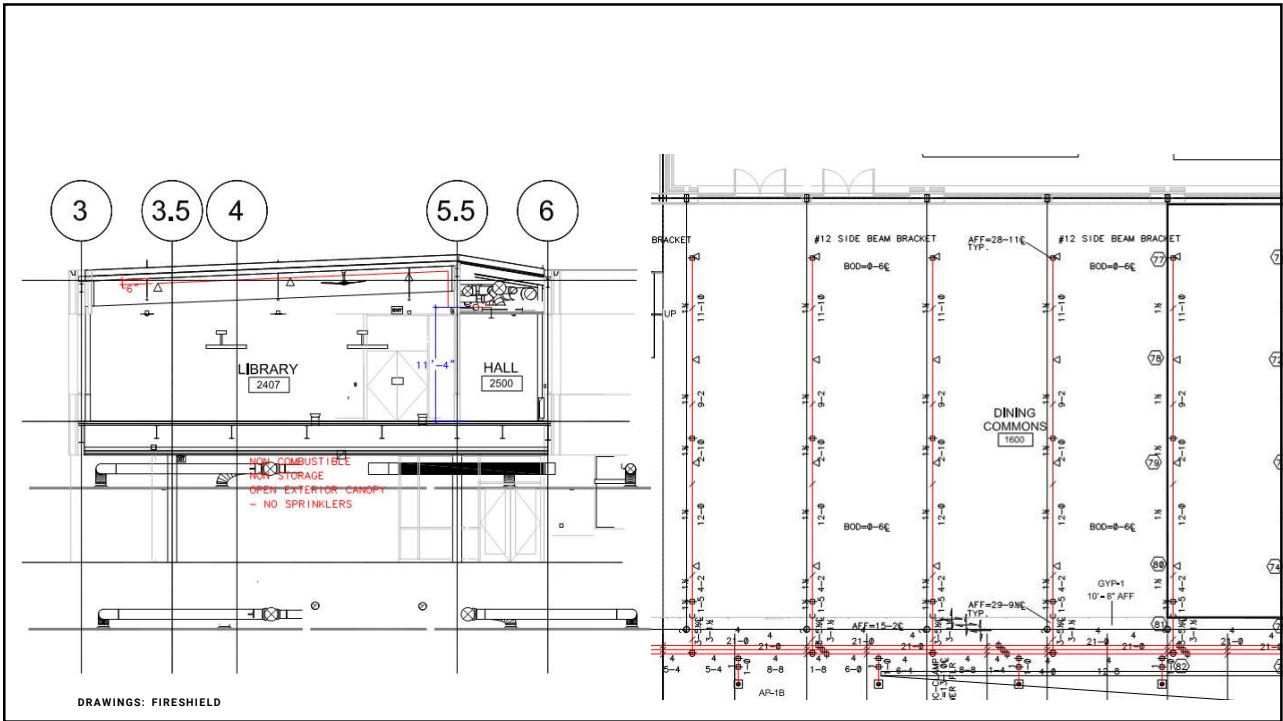
1. NAIL SHEATHING AT ALL PANEL EDGES W/ 10d SPACED PER THE DIAPHRAGM SHEATHING SCHEDULE. FIELD NAIL ALL PANELS W/ 10d @ 12" O.C EA WAY.

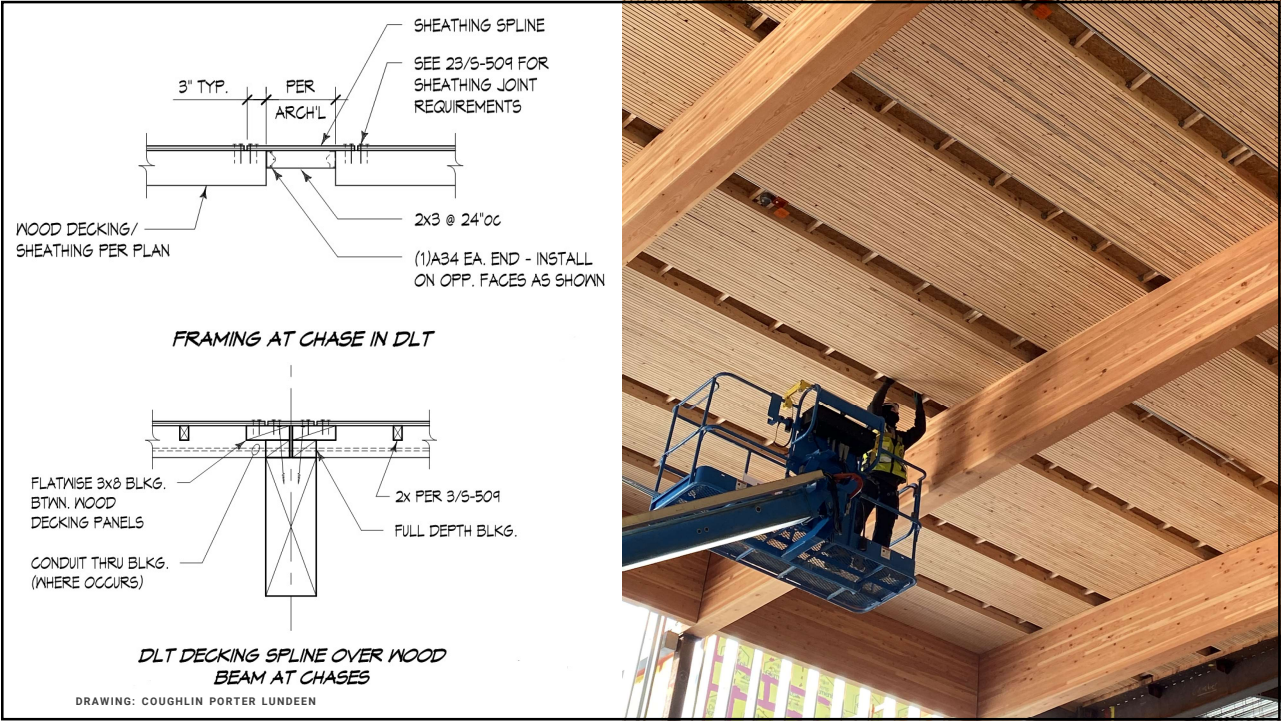
2. SWG SCREWS SHALL BE INSTALLED IN THE CENTER OF DLT LAMINATIONS

DRAWING: STRUCTURCRAFT

CHART: STRUCTURCRAFT



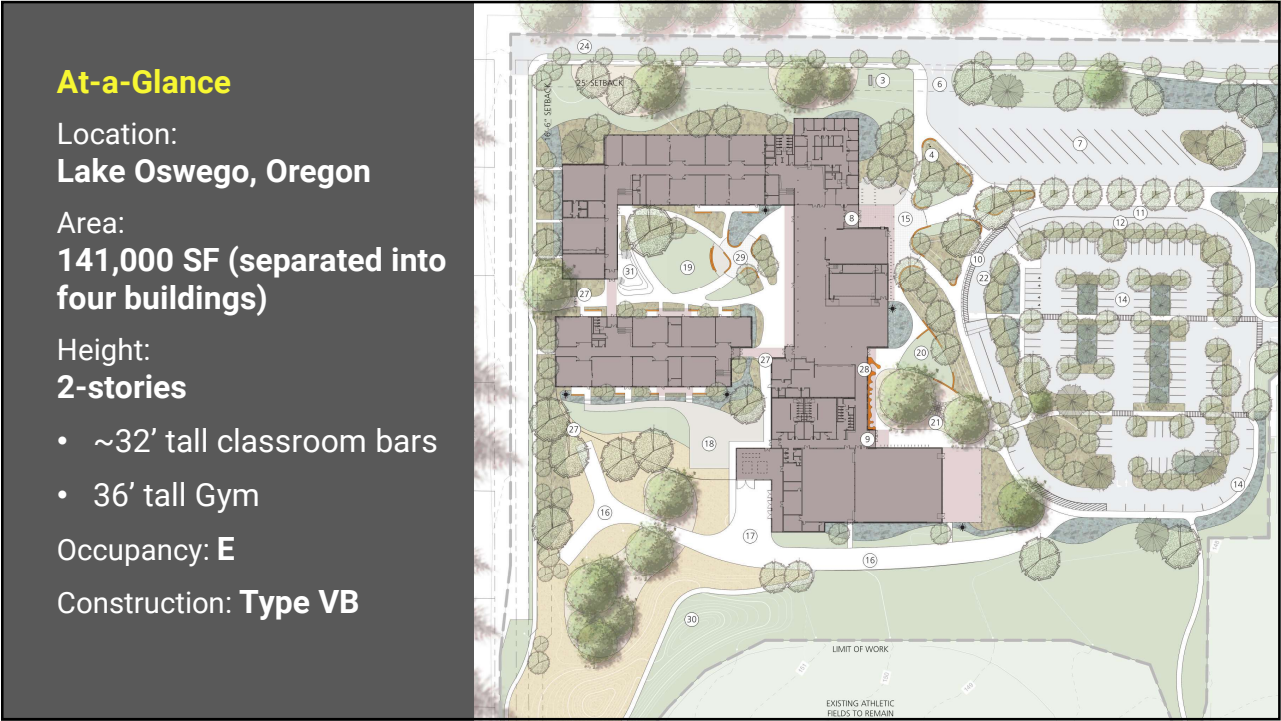


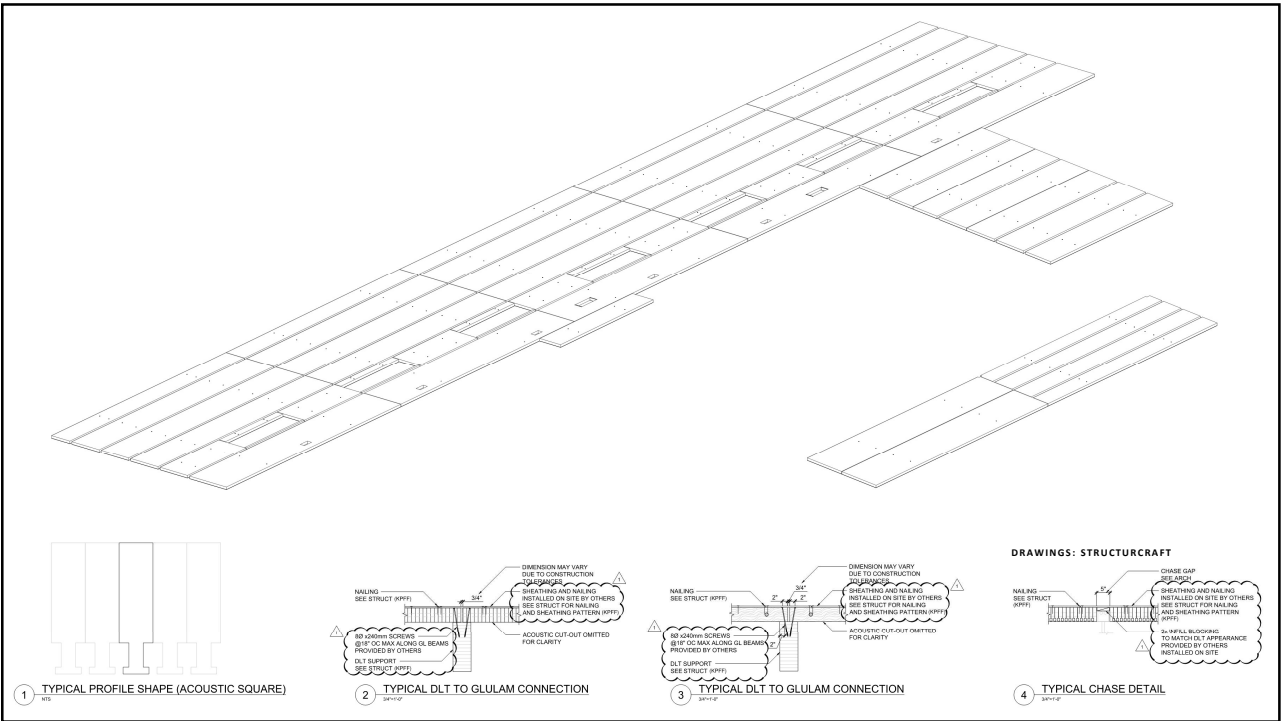


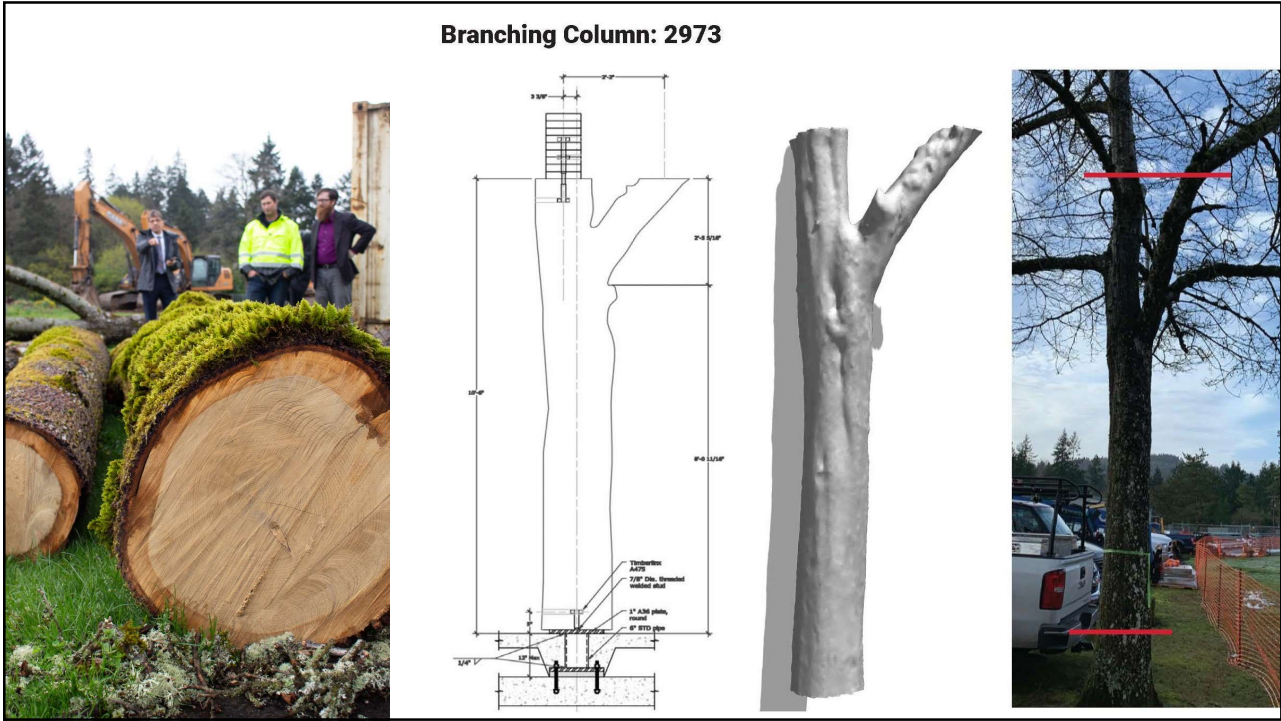
Lakeridge Junior High School

DLT and WholeTrees

2018-Current











The late, great Whatcom Fir

A Douglas fir tree logged a century ago along the North Fork Nooksack River was reputed to be 465 ft. (142 m) tall, which would have made it the tallest tree ever found in North America. Historical reports indicate similar giants grew in the Pacific Northwest, including near the current cities of Seattle and Vancouver, B.C.



IMAGE: WIKIPEDIA

Mass Timber Building Codes

How can we grow the impact of mass timber in Washington State?

ICC Tall Wood Building Committee (established December 2015)

13 Proposals

1. TWB Proposed code changes:
January 2018

2. ICC Committee Action Hearing:
April, 2018

3. ICC Public Comment Hearing:
October, 2018


4. Passed as Proposed by ICC
Membership Vote: December, 2018

977 votes cast


> Votes cast than ever

71% in favor, 29% against

IMAGE: BUILD WITH STRENGTH CAMPAIGN



State-Wide Code Change Proposal



Washington State
Building Code Council

FORT&ERRA

FOR THE PEOPLE. FOR THE LAND. FOREVER.

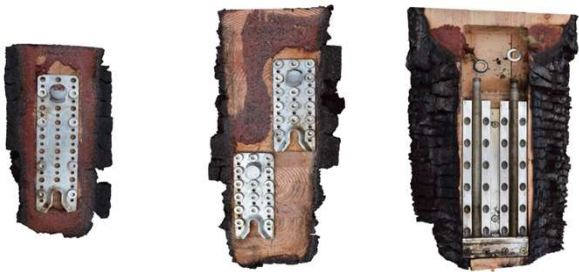
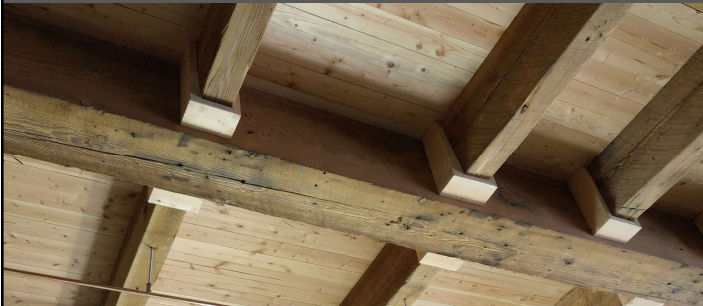
Winter 2018	Spring 2018	Winter 2018	July 2019	July 2020
WA State Legislature passes ESB 5450	Submitted code change proposal to SBCC	SBCC Approves code change proposal	Provisions available for 2015 WA IBC	Provisions available for 2018 IBC
ICC TWB Committee releases proposed code language	SBCC Process and Public Hearings	Pre-adopts 2021 IBC provisions created by TWB		

New Mass Timber Codes

- Type IV-A**
18-story max
- Type IV-B**
12-story max
- Type IV-C**
9-story max
- Type IV-HT**
Don't forget!

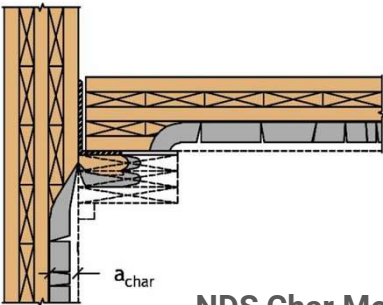
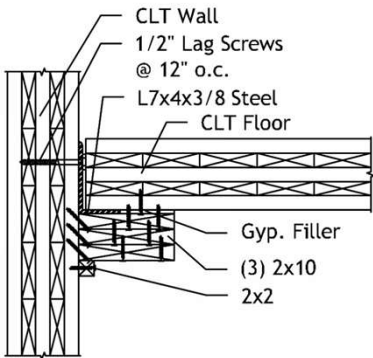
- Concealed spaces allowed with provisions
- All adhesives must be heat resistant (PRG-320 2018)
- Connections must be fire protected
- Exterior walls must be protected
- Tall mass timber requires protection during construction
- Special Inspections

Fire Protection of Connections

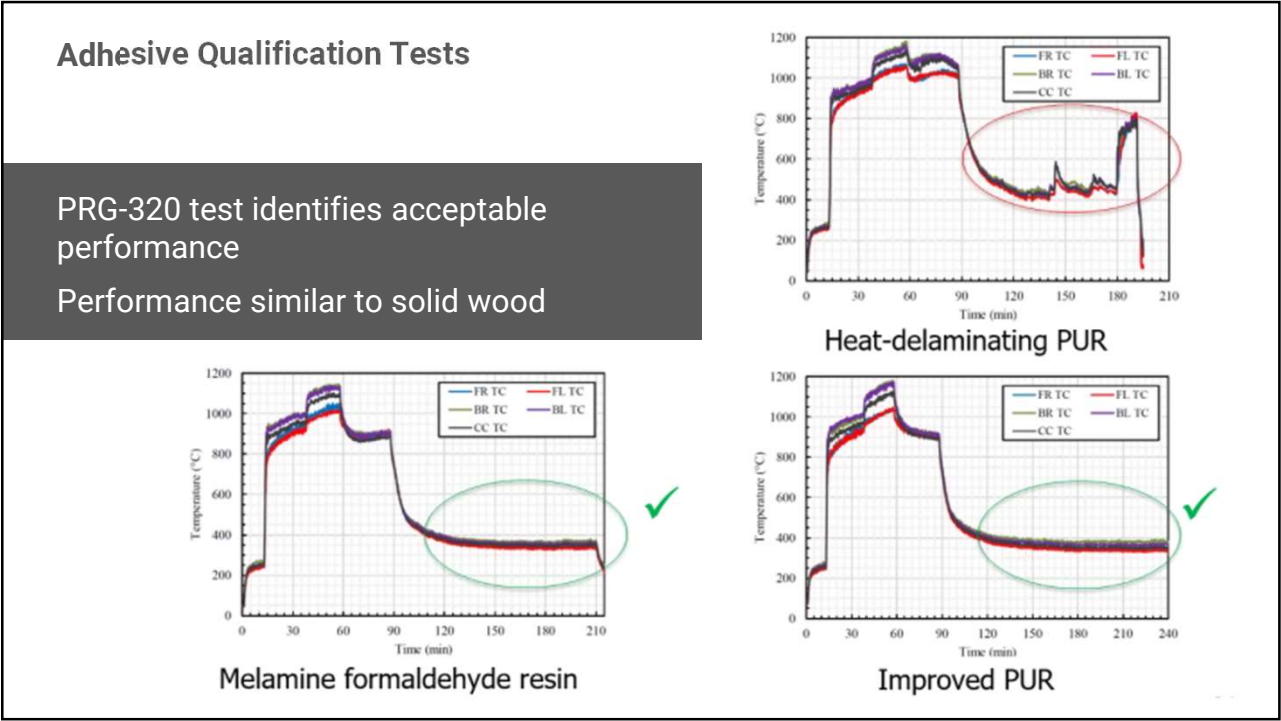


Proprietary Connection Systems

SOURCE: MYTICON



NDS Char Method



Regulatory

- Fire protection of connections – likely handled by Building Official
 - 2018 IBC 110.3.9 and 2021 Chapter 1
 - 2018 IBC 1705.1.1 allows AHJ to require special inspections
- Special Inspections – WABO is finalizing an exam so special inspectors can get registration for this
- Seattle Mass Timber Presubmission Checklist
 - ~2 mass timber presubmissions to date

A construction worker wearing a blue hard hat, a high-visibility yellow safety vest, and a tool belt is kneeling on a wooden roof deck. The worker is using a power tool to install a metal fastener into a wooden beam. The background shows a forested area and a building under construction.

